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CONFIDENCE INTERVALS FOR CEP WHEN THE ERRORS ARE ELLIPTICAL NORMAL

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NOVEMBER 1983

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NAVAL SURFACE WEAPONS CENTER

Dahlgren, Virginia 22448 • Silver Spring, Maryland 20910

ECURITY CLASSIFICATION OF THIS PAGE (When Data Entered

REPORT DOCUMENTATION PAGE READ INSTRUCTIONS					
1. REPORT NUMBER	BEFORE COMPLETING FORM				
NSWC TR 83-205	2. GOVT ACCESSION NO.	3. RECIPIENT'S CATALOG NUMBER			
4. TITLE (and Subtitle)		5 7005 05			
CONFIDENCE INTERVALS FOR CEP WHEN 'ERRORS ARE ELLIPTICAL NORMAL	5. TYPE OF REPORT & PERIOD COVERED Final				
		6. PERFORMING ORG, REPORT NUMBER			
7. AUTHOR(s)		8. CONTRACT OR GRANT NUMBER(4)			
Audrey E. Taub Marlin A. Thomas					
9. PERFORMING ORGANIZATION NAME AND ADDRESS		10. PROGRAM ELEMENT, PROJECT, TASK AREA & WORK UNIT NUMBERS			
Naval Surface Weapons Center		AREA & WORK UNIT NUMBERS			
Code K106		63371N B0951-SB			
Dahlgren, Virginia 22448					
11. CONTROLLING OFFICE NAME AND ADDRESS		12. REPORT DATE			
Strategic Systems Project Office		November 1983			
Washington, D.C. 20376		13. NUMBER OF PAGES 44			
14. MONITORING AGENCY NAME & ADDRESS(If different	from Controlling Office)	15. SECURITY CLASS. (of this report)			
		UNCLASSIFIED			
	15a. DECLASSIFICATION/DOWNGRADING SCHEDULE				
16. DISTRIBUTION STATEMENT (of this Report)					
Approved for public release; distri	bution unlimited	l.			

17. DISTRIBUTION STATEMENT (of the abstract entered in Block 20, if different from Report)

18. SUPPLEMENTARY NOTES

19. KEY WORDS (Continue on reverse side if necessary and identify by block number)

CEP Estimators

CEP Approximations

CEP Confidence Intervals

Elliptical Normal Errors

20. ABSTRACT (Continue on reverse side if necessary and identify by block number)

Approximate confidence intervals are developed for CEP when the delivery errors are elliptical normal. Their accuracies are determined through Monte Carlo sampling. The procedures for confidence interval computation are illustrated via numerical examples.

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FOREWORD

The work documented in this technical report was performed at the Naval Surface Weapons Center (NSWC) by the Mathematical Statistics Staff (K106), Space and Surface Systems Division, Strategic Systems Department. The date of completion was October 1983.

This report was reviewed by Carlton W. Duke, Jr., Head, Space and Surface Systems Division.

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CHAPTER 1

INTRODUCTION

A common parameter for describing the accuracy of a weapon is the circular probable error, generally referred to as CEP. CEP is simply the bivariate analog of the univariate probable error and measures the radius of a mean-centered circle which includes 50% of the bivariate probability. In the case of circular normal errors where the error variances are the same in both directions, CEP can be expressed as a function of the common miss distance standard deviation. Also, CEP estimators based on observed miss distances are easily formulated and can be used to construct confidence intervals for CEP. In the case of elliptical normal errors, CEP cannot be expressed explicitly as a function of the miss distance standard deviations. Here, one must obtain CEP by numerical methods or by referring to tabular values. This has led to the development of a number of approximations by which CEP can be expressed as a function of the miss distance standard deviations. While CEP estimators based on observed miss distances are easily formulated from these approximations, their probability distributions are too complicated to be useful for CEP confidence intervals. In this report, these probability distributions are approximated with distributions which are more practical for the formulation and application of CEP confidence intervals. proximate CEP confidence intervals are then formulated and their accuracy determined through Monte Carlo sampling.

The first part of this report is tutorial in the development of CEP and discusses the commonly used approximations for the elliptical case. The development of approximate confidence intervals begins with Chapter 4.

CHAPTER 2

REVIEW OF CIRCULAR CASE

In general, it will be assumed that the errors in the X and Y directions are independent with mean zero and variances σ_x^2 and σ_y^2 , respectively. Under the circular normal assumption, $\sigma_x^2 = \sigma_y^2 = \sigma^2$ and the bivariate distribution of errors is given by

$$f_c(x,y) = \frac{1}{2\pi\sigma^2} e^{-(x^2 + y^2)/2\sigma^2}$$
, $-\infty < x, y < \infty$ (2.1)

where the subscript c denotes circular. The distribution of the radial miss distance is derived by first obtaining the distribution of the polar variables $(R,\;\theta)$ where

 $X = R \cos \Theta$

 $Y = R \sin \Theta$.

This is found to be

$$g_c(r,\theta) = \frac{r}{2\pi\sigma^2} e^{-r^2/2\sigma^2}, 0 < r < \infty, 0 < \theta < 2\pi.$$
 (2.2)

The distribution of $R = (X^2 + Y^2)^{\frac{1}{2}}$ is now obtained from (2.2) by using the marginal rule; i.e.,

$$g_{c}(r) = \int_{0}^{2\pi} g_{c}(r,\theta) d\theta = \frac{r}{\sigma^{2}} e^{-r^{2}/2\sigma^{2}}, r > 0.$$
 (2.3)

This is the well-known Rayleigh distribution (see Lindgren (1968)) with cumulative distribution function

$$P(R < r) = G_c(r) = 1 - e^{-r^2/2\sigma^2}$$
 (2.4)

By definition, $G_{\rm C}({\rm CEP})$ = .5 and the solution of (2.4) yield the frequently used expression

CEP =
$$[-2 \ln(.50)]^{\frac{1}{2}} \sigma = 1.1774 \sigma.$$
 (2.5)

Consider now that σ (and hence, CEP) is unknown and is estimated from n observed miss distances. These miss distances will be designated as (x_i, y_i) , $i = 1, \ldots, n$ in the X and Y directions, respectively. Moranda (1959) has shown that the maximum likelihood estimator for σ is

$$\hat{\sigma} = \left\{ \sum_{i=1}^{n} (x_i^2 + y_i^2)/2n \right\}^{\frac{1}{2}}, \tag{2.6}$$

and the corresponding estimator for CEP is simply $\stackrel{\circ}{\text{CEP}} = 1.1774 \stackrel{\circ}{\text{O}}$. This estimator is biased for CEP, i.e., the expectation of CEP is not equal to CEP. However, the bias is small and the unbiasing factor is cumbersome. Therefore, it will be retained in its slightly biased form.

To place confidence limits on CEP, it will be necessary to examine the probability distribution of CEP. It is well-known under normal theory (see Mood and Graybill (1963)) that if $\{W_i\}$, $i=1,\ldots,n$ is a random sample from a normal population with mean μ and variance σ^2 , then $\Sigma(W_i - \mu)^2/\sigma^2$ has a chi-square distribution with n degrees of freedom. One can consider $\{x_i\}$, $i=1,\ldots,n$ and $\{y_i\}$, $i=1,\ldots,n$ to be a random sample of size 2n from a normal population with mean zero and variance σ^2 . Therefore,

$$\sum_{i=1}^{n} \frac{\left(x_{i}^{2} + y_{i}^{2}\right)}{\sigma^{2}} = \frac{2n\hat{\sigma}^{2}}{\sigma^{2}} = \frac{2n\hat{CEP}^{2}}{CEP^{2}} \sim \chi_{2n}^{2}$$
(2.7)

where "~" designates "is distributed as" and χ^2_{2n} designates a chi-square probability distribution with 2n degrees of freedom. The 100 (1 - α)% confidence limits are now easily constructed using the probability statement

$$\Pr \left\{ \begin{array}{l} \chi_{2n,\alpha/2}^{2} < \frac{2n\hat{CEP}^{2}}{CEP^{2}} < \chi_{2n,1-\alpha/2} \end{array} \right\} = 1 - \alpha \quad . \tag{2.8}$$

In this expression, $\chi^2_{\upsilon,\alpha}$ designates the 100 α percentage point for a chi-square with υ degrees of freedom. Tabular values for integral υ can be found in the back of most statistics texts. A more complete table is found in Hald (1952). Manipulating the inequality in (2.8) leads to the following 100 (1 - α)% confidence limits for CEP:

$$\left[\frac{\hat{\text{CEP}}}{(\chi_{2n,1-\alpha/2}^{2/2n})^{\frac{1}{2}}}, \frac{\hat{\text{CEP}}}{(\chi_{2n,\alpha/2}^{2/2n})^{\frac{1}{2}}} \right] . \tag{2.9}$$

The interpretation here is that one is 100 (1 - α)% confident that the interval in (2.9) contains the population CEP. This formula is valid only for the case where the errors are known to be circular, i.e., the case where $\sigma_x^2 = \sigma_y^2 = \sigma^2$.

Before leaving this review of the circular case, it will be instructive to work through an example. Suppose confidence limits on CEP are desired from the ten round sample shown in Table 2-1. We first need to compute $\hat{\sigma}$ in (2.6). One notes that the sum under the radical in (2.6) can be expressed as

$$\left(\frac{\sum x_i^2}{n} + \frac{\sum y_i^2}{n}\right)/2$$
.

TABLE 2-1. 10 HYPOTHETICAL MISS DISTANCES (FEET)

X	$\underline{\mathbf{y}}$
42	-123
-13	-12
-50	14
-70	169
-191	-58
117	- 79
158	99
16	-18
101	170
27	65

The two components are independent estimates of the common variance σ^2 . If they differ significantly, it would cast doubt on the circular normal assumption. These components will be referred to as s_x^2 and s_y^2 so that $\hat{\sigma}$ in (2.6) becomes

$$\hat{\sigma} = \left[\left(s_{\mathbf{x}}^2 + s_{\mathbf{y}}^2 \right) / 2 \right]^{\frac{1}{2}}.$$

For this example, one finds

$$s_x^2 = \sum x_i^2/n = 9565.3$$

 $s_y^2 = \sum y_i^2/n = 9688.5$
 $\hat{\sigma} = [(9565.3 + 9688.5)/2]^{\frac{1}{2}} = 98.12$
 $\hat{CEP} = 1.1774 \hat{\sigma} = 115.53.$

To form confidence limits, the computations in (2.9) are required. Let us consider 95% limits so α = .05 and the tabular values required are

$$\chi^{2}_{20,.025} = 9.59$$

 $\chi^{2}_{20,.975} = 34.20$.

These would both be divided by 2n = 20 to form the terms under the radical in (2.9). One could also use a table of chi-square percentage points divided by the degrees of freedom here to avoid the latter step. Such a table is in Hald (1952) and provides

$$\chi^{2}_{20,.025}/20 = .4796$$
 $\chi^{2}_{20,.975}/20 = 1.7085$

The 95% confidence limits on CEP can now be completed and are found to be

$$\left(\frac{115.53}{(1.7085)^{\frac{1}{2}}}, \frac{115.53}{(.4796)^{\frac{1}{2}}}\right) = (88.39, 166.82)$$

The units are feet, the same as the miss distance units in Table 2-1. The interpretation is that one is 95% confident that the true (or population) CEP lies in the interval (88.39, 166.82). The result is valid only if the probability distribution of miss distances follows a circular normal distribution. Application of (2.9) when the probability distribution is elliptical can lead to serious errors. A discussion of the elliptical case begins with Chapter 3.

CHAPTER 3

CEP DERIVATION AND APPROXIMATIONS FOR ELLIPTICAL ERRORS

In the elliptical case, the error variances are unequal and the bivariate distribution of errors is given by

$$f_{E}(x,y) = \frac{1}{2\pi\sigma_{x}\sigma_{y}} e^{-\frac{1}{2}[(x/\sigma_{x})^{2} + (y/\sigma_{y})^{2}]}, - \infty < x,y < \infty$$

where the subscript E denotes elliptical. The distribution of the radial error R for this case was derived by Chew and Boyce (1961). They proceeded, as in the circular case, by first obtaining the distribution of the polar variables (R,θ) . This was found to be

$$g_{E}(r,\theta) = \frac{r}{2\pi\sigma_{x}\sigma_{y}} e^{-ar^{2}} e^{(-br^{2}\cos 2\theta)}, \quad 0 < r < \infty \\ 0 < \theta < 2\pi$$
 (3.1)

where

$$a = \frac{\sigma_y^2 + \sigma_x^2}{(2\sigma_x\sigma_y)^2}, b = \frac{\sigma_y^2 - \sigma_x^2}{(2\sigma_x\sigma_y)^2}.$$

Using the marginal rule, the distribution of R was obtained by integrating $g_{E}(r,\theta)$ in (3.1) with respect to θ between 0 and 2π . This integration cannot be expressed in tractable form, so they expressed their result in terms of a modified Bessel function as

$$g_{E}(r) = \frac{r}{\sigma_{x}\sigma_{y}} e^{-ar^{2}} I_{0}(br^{2}), 0 < r < \infty$$
 (3.2)

In this expression, the subscript E denotes elliptical and I_0 is a modified Bessel function of the first kind and zero order, i.e.,

$$I_0(x) = \frac{1}{\pi} \int_0^{\pi} e^{-x\cos\theta} d\theta.$$

The cumulative distribution function for R is denoted by

$$P(R < r) = G_E(r) = \int_0^r g_E(t) dt.$$
 (3.3)

However, $G_E(r)$ cannot be expressed in tractable form because $g_E(t)$ cannot be so expressed. This means that the radius of the 50% circle for the elliptical case cannot be expressed by a simple formula as it was in the circular case. One has to solve $G_E(CEP) = .5$ by numerical methods or by referring to tables prepared by Harter (1960), DiDonato and Jarnagin (1962), and others. To avoid using these tables or numerical procedures for CEP evaluation, a number of approximations have been developed over the years. Five of the most common are shown below; they are designated as CEP_1 through CEP_5 :

$$\begin{aligned} \text{CEP}_1 &= 1.1774 \left(\frac{\sigma_x^2 + \sigma_y^2}{2} \right)^{\frac{1}{2}} \\ \text{CEP}_2 &= 1.1774 \left(\frac{\sigma_x + \sigma_y}{2} \right) \\ \text{CEP}_3 &= \left(2 \ \chi_{0,.50}^2 / \upsilon \right)^{\frac{1}{2}} \left(\frac{\sigma_x^2 + \sigma_y^2}{2} \right)^{\frac{1}{2}} \\ \upsilon &= \frac{\left(\sigma_x^2 + \sigma_y^2 \right)^2}{\sigma_x^4 + \sigma_y^4} \\ \text{CEP}_4 &= .565 \ \sigma_{\text{max}} + .612 \ \sigma_{\text{min}}, \ \sigma_{\text{min}} / \sigma_{\text{max}} &\geq .25 \\ &= .667 \ \sigma_{\text{max}} + .206 \ \sigma_{\text{min}}, \ \sigma_{\text{min}} / \sigma_{\text{max}} &< .25 \\ \text{CEP}_5 &= \left[2^{\frac{1}{3}} \left(1 - \frac{2}{9\upsilon} \right) \right]^{\frac{3}{2}} \left(\frac{\sigma_x^2 + \sigma_y^2}{2} \right)^{\frac{1}{2}} . \end{aligned}$$

CEP₁ and CEP₂ were taken from Groves (1961); CEP₃ was formulated using the chisquare approximation for calculating hit probabilities provided by Grubbs (1964). It was also derived independent of the Grubbs approximation by Thomas and Taub (1978). CEP₄ is a piece-wise linear combination of standard deviations which is commonly used in the missile community; CEP₅ was formulated by Terzian (1974) using the Wilson-Hilferty approximation for calculating hit probabilities provided by Grubbs (1964). Plots of each approximation versus the true CEP as a function of $\sigma_{\min}/\sigma_{\max}$ are shown in Figures 3-1 through 3-5. These give a fairly good indication of how well each performs. It is seen that CEP₁ deteriorates rapidly as we depart from the circular case (for which CEP₁ degenerates to 1.1774 σ), CEP₂ is reasonably good if the ratio $\sigma_{\min}/\sigma_{\max}$ is not less than about .2; CEP₃ appears good for all ratios, and CEP₄ and CEP₅ appear good to a lesser extent for all ratios.

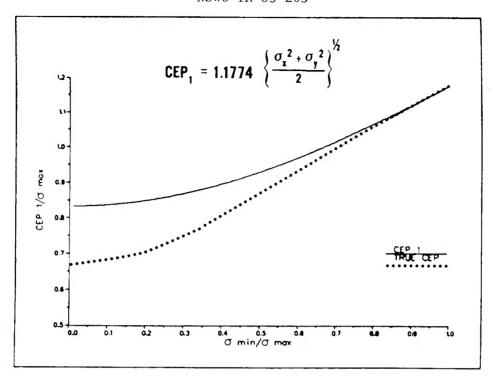


FIGURE 3-1. CEP_1 APPROXIMATION VERSUS TRUE CEP

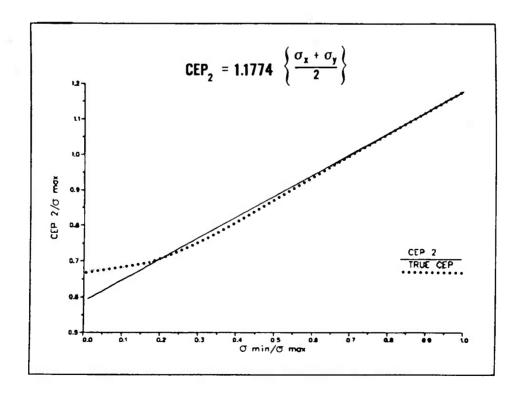


FIGURE 3-2. CEP_2 APPROXIMATION VERSUS TRUE CEP

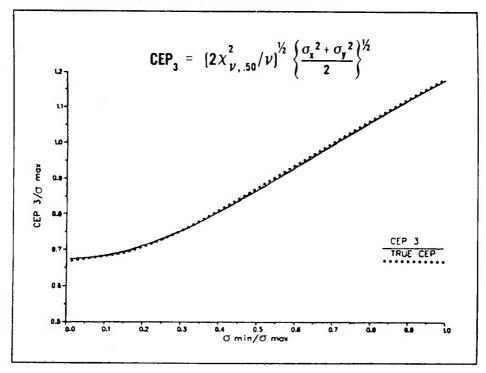


FIGURE 3-3. ${\tt CEP_3}$ APPROXIMATION VERSUS TRUE CEP

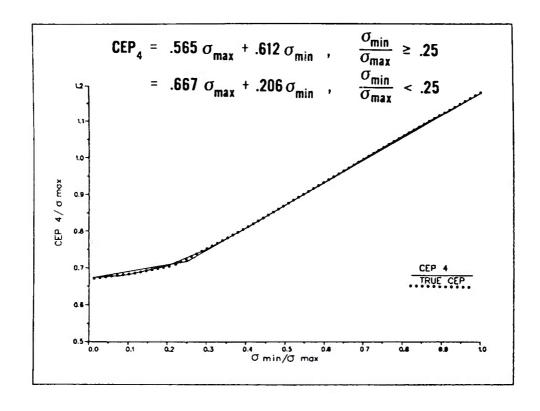


FIGURE 3-4. CEP_4 APPROXIMATION VERSUS TRUE CEP

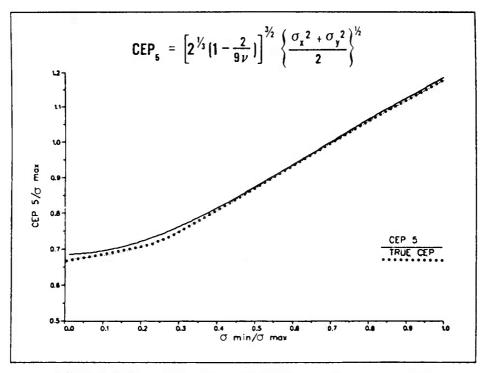


FIGURE 3-5. CEP₅ APPROXIMATION VERSUS TRUE CEP

To recap the elliptical case thus far, for known values of σ_x and σ_y , one can compute the exact CEP by solving $G_E(\text{CEP})=.50$ or compute an approximate CEP by using an approximation such as CEP₁ to CEP₅. Consider now that σ_x and σ_y (and hence CEP) are unknown and are to be estimated from n observed miss distances. These miss distances will be designated as before, as $(\mathbf{x_i},\mathbf{y_i})$, $\mathbf{i}=1,\ldots,n$ in the X and Y directions, respectively. The maximum likelihood estimators for σ_x and σ_y pose no problem. They are given by

$$s_{x} = \hat{\sigma}_{x} = \left\{ \sum_{i=1}^{n} x_{i}^{2}/n \right\}^{\frac{1}{2}}, \quad s_{y} = \hat{\sigma}_{y} = \left\{ \sum_{i=1}^{n} y_{i}^{2}/n \right\}^{\frac{1}{2}}$$
(3.4)

as shown in Lindgren (1968). These estimators are slightly biased and as before, they will not be corrected due to the cumbersome nature of the correction factor. They can now be substituted for the unknown $\sigma's$ in (3.3) to obtain a numerical estimate of CEP by solving $G_{\underline{E}}(\text{CEP})=.50$ or they can be substituted into CEP $_1$ to CEP $_5$ to obtain estimates of the approximate CEP. These latter estimators will be referred to as CEP $_1$ to CEP $_5$ and have the appeal of being explicitly expressible. Hence, estimates of CEP for the elliptical case can be rather easily obtained.

The problem of obtaining confidence limits for CEP in this case is more complex. The complexity is based on the fact that to find confidence limits for a parameter, one needs information regarding the probability distribution of the estimator for the parameter. As previously noted, CEP can be obtained by solving $G_{\underline{E}}(CEP) = .50$. Symbolically, we can write

$$\hat{CEP} = G_E^{-1} (.50)$$
 (3.5)

but to obtain it requires recursive numerical integration or the use of previously noted tables. Hence, the formulation of confidence limits based on this estimator holds little promise for a practical solution. Therefore, we shall consider the formulation of confidence limits based on the estimators of the approximate CEP. The distributions of these estimators are extremely complicated since they involve radicals and linear combinations of sample variances and standard deviations. Hence, these distributions were approximated and confidence limits formulated on the basis of the approximate distributions. This development is provided in Chapter 4.

CHAPTER 4

APPROXIMATE DISTRIBUTIONS OF CEP ESTIMATORS

The five estimators for CEP fall into two classes. One class involves the square root of linear combinations of sample variances and the other involves linear combinations of sample standard deviations. $\widehat{\text{CEP}}_1$, $\widehat{\text{CEP}}_3$, and $\widehat{\text{CEP}}_5$ fall into the first class and can be written in the form

$$CEP_{i} = K_{i} \frac{(s_{x}^{2} + s_{y}^{2})^{\frac{1}{2}}}{2}, i = 1, 3, 5$$
 (4.1)

where

$$K_1 = 1.1774$$

$$K_3 = \left(2 \chi_{0,.50}^2 / \upsilon\right)^{\frac{1}{2}}$$

$$K_5 = \left[2^{1/3} (1 - 2/9\upsilon)\right]^{3/2} .$$

CEP₂ and CEP₄ fall into the second class and can be written in the form

$$CEP_i = a_1 s_{max} + a_2 s_{min}, i = 2, 4$$
 (4.2)

where for i = 2, $a_1 = a_2 = 1.1774/2$

and for
$$i = 4$$
, $a_1 = .565$ and $a_2 = .612$ when $s_{min}/s_{max} \ge .25$
 $a_1 = .667$ and $a_2 = .206$ when $s_{min}/s_{max} < .25$.

The distribution of the square of each estimator can be approximated by a chi-square distribution with appropriate degrees of freedom. The following is the rationale for these approximations. The squares of $\widehat{\text{CEP}}_1$, $\widehat{\text{CEP}}_3$, and $\widehat{\text{CEP}}_5$ are linear combinations of sample variances. Satterthwaite (1946) has shown that one can approximate the distribution of such linear combinations with a chi-square distribution with degrees of freedom chosen so the approximate distribution has a variance equal to that of the exact distribution. Here, one is approximating the distribution of a linear combination of sample variances with a chi-square. A natural extension is to approximate the distribution of a linear combination of sample standard deviations with a chi-distribution (see Appendix C). Hence, the distributions of $\widehat{\text{CEP}}_2$ and $\widehat{\text{CEP}}_4$ were approximated by a chi-distribution with degrees of freedom chosen so the approximate distribution has a variance equal

to that of the exact distribution. Since the square of a chi-variable has a chi-square distribution, the squares of $\widehat{\text{CEP}}_2$ and $\widehat{\text{CEP}}_4$ also have approximate chi-square distributions. The major task is to find the appropriate degrees of freedom for each class of estimator.

First, one sees that CEP_1 has the same form as the maximum likelihood estimator for CEP in the circular case. In that case, the degrees of freedom associated with CEP were 2n. These same degrees of freedom will be retained here for CEP_1 . This will eventually show how poorly CEP_1 performs as an estimator for CEP when the error distribution is elliptical vice circular.

Next, consider CEP₃ and CEP₅ of the first class. Each has form

$$CEP_{i} = K_{i} \left(\frac{s_{x}^{2} + s_{y}^{2}}{2} \right)^{\frac{1}{2}}$$
.

To obtain υ' , the degrees of freedom for our chi-square, we need to equate the variance of $\upsilon' \hat{\text{CEP}}_i^2/\text{CEP}_i^2$ with $2\upsilon'$ (the variance of a chi-square with υ' degrees of freedom) and solve for υ' . Now

$$\frac{\upsilon' \stackrel{\frown}{CEP_{i}^{2}}}{CEP_{i}^{2}} = \frac{\upsilon' \quad K_{i}^{2} \left(s_{x}^{2} + s_{y}^{2}\right)}{2 \quad CEP_{i}^{2}}$$

and the variance of this expression is

$$\frac{(\upsilon')^2 K_i^4}{4 \text{ CEP}_i^4} \left(\frac{2\sigma_x^4}{n} + \frac{2\sigma_y^4}{n} \right).$$

Upon substituting $K_{i} \left(\frac{\sigma_{x}^{2} + \sigma_{y}^{2}}{2} \right)^{\frac{1}{2}}$ for CEP_i, this becomes

$$\frac{(\upsilon')^2 \left(\sigma_x^4 + \sigma_y^4\right)}{n\left(\sigma_x^2 + \sigma_y^2\right)^2}$$

Equating this expression to $2\upsilon'$ and solving for υ' yields

$$\upsilon' = \frac{n\left(\sigma_x^2 + \sigma_y^2\right)^2}{\left(\sigma_x^4 + \sigma_y^4\right)} = n \ \upsilon \tag{4.3}$$

where υ was previously defined to be

$$v = \frac{\left(\sigma_{x}^{2} + \sigma_{y}^{2}\right)^{2}}{\sigma_{x}^{4} + \sigma_{y}^{4}} . \tag{4.4}$$

Consider next, CEP_2 and CEP_4 of the second class. Each of these estimators has the form

$$\widehat{CEP}_{i} = a_{1} s_{max} + a_{2} s_{min}$$
 $i = 2, 4$.

To obtain 0th, the degrees of freedom for the chi-square in this class, we equate

the variance of
$$\frac{\left(\upsilon^{*}\right)^{\frac{1}{2}}\hat{CEP}_{i}}{CEP_{i}}$$
 with υ^{*} - $2\left[\frac{\Gamma\left(\frac{\upsilon^{*}+1}{2}\right)}{\Gamma\left(\frac{\upsilon^{*}}{2}\right)}\right]^{2}$ (the variance of a chi-random

variable with o' degrees of freedom) and solve for o'. Now,

$$\frac{\left(\upsilon^{*}\right)^{\frac{1}{2}}\hat{CEP}_{i}}{CEP_{i}} = \frac{\left(\upsilon^{*}\right)^{\frac{1}{2}}\left(a_{1} s_{\max} + a_{2} s_{\min}\right)}{\left(a_{1} \sigma_{\max} + a_{2} \sigma_{\min}\right)}$$

and the variance of this expression is

$$\frac{\upsilon^{\frac{1}{2}} \left(a_{1}^{2} V\left(s_{\max}\right) + a_{2}^{2} V\left(s_{\min}\right)\right)}{\left(a_{1} \sigma_{\max} + a_{2} \sigma_{\min}\right)^{2}}.$$
(4.5)

If we denote the function H(x) as

$$H(x) = \sqrt{\frac{2}{x}} \frac{\Gamma\left(\frac{x+1}{2}\right)}{\Gamma\left(\frac{x}{2}\right)}, \qquad (4.6)$$

then the variance of a sample standard deviation based on n observations, i.e., the variance of s $_{\rm X}$ or s $_{\rm V}$ shown in (3.4) can be expressed as

$$V(s_x) = V(s_y) = \sigma^2 [1 - H^2(n)].$$

Using this notation in (4.5) and equating the latter to the variance of a chirandom variable yields

$$\frac{\left(a_1^2 \sigma_X^2 + a_2^2 \sigma_y^2\right) \left(1 - H^2(n)\right)}{\left(a_1 \sigma_X + a_2 \sigma_y\right)^2} = 1 - H^2(v^*)$$

or

$$H(v^{\frac{1}{2}}) = \left[1 - \left\{1 - H^{2}(n)\right\} \frac{\left(a_{1}^{2} \sigma_{x}^{2} + a_{2}^{2} \sigma_{y}^{2}\right)}{\left(a_{1} \sigma_{x} + a_{2} \sigma_{y}\right)^{2}}\right]^{\frac{1}{2}}.$$
(4.7)

The value of υ^{k} cannot be computed explicitly but is easily obtained using the following procedure.

Evaluate the right-hand side of (4.7) using estimates of σ_x and σ_y obtained from n sample data points and values of a_1 and a_2 determined by (4.2). Call this value w. Refer to Appendix B which contains tabled values of x and H(x). Enter the table and find the value of x for which H(x) = w. This value of x is $\upsilon^{\frac{1}{4}}$. An example which incorporates this procedure begins in Chapter 5.

Clearly, υ' and υ^* may take on fractional (non-integral) values. However, this poses no problem. Although the question of fractional degrees of freedom is rarely addressed in standard statistics texts, an extensive table of chisquare percentage points with fractional degrees of freedom has been generated by DiDonato and Hageman (1977). Also, one can obtain such percentage points using the MDCHI subroutine available in IMSL (1982).

For each of the five CEP estimators, it has been shown that the distribution of

$$\frac{v_i \hat{CEP}_i^2}{CEP_i^2}$$
 $i = 1, 2, ... 5$ (4.8)

can be approximated by a chi-square distribution with υ_i degrees of freedom where υ_i is either 2n, υ' , or υ^* defined previously. Since the form of a confidence interval for a chi-square random variable is well-known, construction of confidence intervals for CEP, using (4.8), is straightforward.

CHAPTER 5

APPROXIMATE CEP CONFIDENCE INTERVALS

An approximate 100 (1 - α)% confidence interval for the true (population) CEP can be constructed using the probability statement

$$\operatorname{Prob}\left\{\chi_{\upsilon_{i}}^{2}, \alpha/2 < \frac{\upsilon_{i} \stackrel{\frown}{\operatorname{CEP}_{i}^{2}}}{\operatorname{CEP}_{i}^{2}} < \chi_{\upsilon_{i}}^{2}, 1-\alpha/2\right\} = 1 - \alpha . \tag{5.1}$$

The subscript i is used to indicate the approximation on which the estimate \overrightarrow{CEP}_i and the degrees of freedom, υ_i , are based. Rewriting (5.1) in terms of \overrightarrow{CEP}_i yields

$$\left(\frac{\widehat{\operatorname{CEP}}_{i}}{\left(\chi_{\upsilon_{i},1-\alpha/2}^{2}/\upsilon_{i}\right)^{\frac{1}{2}}} < \widehat{\operatorname{CEP}}_{i} < \frac{\widehat{\operatorname{CEP}}_{i}}{\left(\chi_{\upsilon_{i},\alpha/2}^{2}/\upsilon_{i}\right)^{\frac{1}{2}}}\right).$$
(5.2)

However, CEP_{i} represents an approximation to the true CEP for any i. Therefore, (5.2) may be considered an approximate confidence interval for CEP and expressed as

$$\left(\frac{\hat{\operatorname{CEP}}_{i}}{\left(\chi_{\upsilon_{i},1-\alpha/2}^{2}/\upsilon_{i}\right)^{\frac{1}{2}}} < \operatorname{CEP} < \hat{\left(\chi_{\upsilon_{i},\alpha/2}^{2}/\upsilon_{i}\right)^{\frac{1}{2}}}\right) .$$
(5.3)

In the following example, approximate confidence intervals will be computed for CEP using two CEP estimators, CEP $_3$ and CEP $_4$. Using (3.4), estimates of $\sigma_{_X}$ and $\sigma_{_Y}$ can be computed for the 12 sample miss distances given in Table 5-1.

TABLE 5-1. 12 HYPOTHETICAL MISS DISTANCES (FEET)

X	<u>y</u>
-163	-363
104	- 56
-47	224
- 13	-61
-84	-267
53	-85
93	383

TABLE 5-1. (Cont.)

X	<u>y</u>
197	-147
-266	61
135	626
107	187
-112	-11

For these data, one finds

$$s_x^2 = \sum_{i=1}^n x_i^2/n = 17,505.00$$

$$s_y^2 = \sum_{i=1}^n y_i^2/n = 72,191.75$$
.

As previously defined,

$$\hat{CEP}_3 = \left(2\chi_{0,.50}^2/\nu\right)^{\frac{1}{2}} \left(\frac{s_x^2 + s_y^2}{2}\right)^{\frac{1}{2}} .$$

Since υ assumes values between 1 and 2 inclusively, a table of the $(2\chi_{\upsilon,.50}/\upsilon)^{\frac{1}{2}}$ factor is readily constructed using chi-square percentage points taken from DiDonato and Hageman (1977). Table 5-2 is a short table that has been prepared to facilitate computation.

TABLE 5-2. MULTIPLYING FACTORS OF $\left(\frac{s_x^2 + s_y^2}{2}\right)^{\frac{1}{2}}$ FOR CEP₃ APPROXIMATION

υ	$\left(2 \chi_{0,.50}^{2}/\nu\right)^{\frac{1}{2}}$
1.0	.9538
1.1	.9928
1.2	1.0258
1.3	1.0542
1.4	1.0789
1.5	1.1005
1.6	1.1195
1.7	1.1365
1.8	1.1516
1.9	1.1652
2.0	1.1774

$$\upsilon = \frac{\left(\sigma_x^2 + \sigma_y^2\right)^2}{\sigma_x^4 + \sigma_y^4}$$

The 12 sample miss distances in Table 5-1 are used to obtain estimates of υ and υ' given by $\hat{\upsilon}$ and $\hat{\upsilon}'$ below:

$$\hat{v} = \frac{\left(s_{X}^{2} + s_{Y}^{2}\right)^{2}}{s_{X}^{4} + s_{Y}^{4}} = 1.46 \qquad \hat{v}' = \hat{n}\hat{v} = 17.52 .$$

Interpolation in Table 5-2 gives $\left(2 \chi_{\hat{0},.50}^2/\hat{v}\right)^{\frac{1}{2}} = 1.0919$ so that

$$CEP_3 = (1.0919) (211.77) = 231.23$$
.

To form confidence limits, the computations in (5.3) are needed. If 95% limits are considered, the chi-square tabular values for α = .05 are obtained via interpolation in DiDonato and Hageman (1977) and are

$$\chi^2_{\hat{v}', ..025} = 7.91$$

$$\chi^2_{\hat{0}}$$
, $975 = 30.89$.

The approximate 95% confidence interval for CEP based on approximation 3 is, therefore

$$\left(\frac{231.23}{(30.89/17.52)^{\frac{1}{2}}} < CEP < \frac{231.23}{(7.91/17.52)^{\frac{1}{2}}}\right)$$

or

$$(174.14 < CEP < 344.13)$$
.

The interpretation here is that one is approximately 95% confident that the true CEP lies in the computed interval.

Let us next consider the approximate 95% confidence interval obtained by using $\widehat{\text{CEP}}_4$. Before using estimator 4, one must compute the ratio $c = s_{\min}/s_{\max}$ to determine which half of the piece-wise approximation should be used. In this case, c = .49 so that

$$\hat{CEP}_4 = .565 \text{ s}_{max} + .612 \text{ s}_{min} = 232.78.$$

This is reasonably close to the 231.23 obtained for CEP $_3$.

To determine υ^* , an estimate of υ^* , evaluate

$$\hat{H(0^{\frac{1}{N}})} = \left[1 - (1 - H^{2}(n)) \frac{\left(.\overline{565}^{2} s_{max}^{2} + .\overline{612}^{2} s_{min}^{2}\right)\right]^{\frac{1}{2}}}{\left(.565 s_{max}^{2} + .612 s_{min}^{2}\right)^{2}}.$$

 $\mathrm{H}^2(\mathrm{n})$ may be determined using tabled values of the gamma function provided in the National Bureau of Standards Applied Mathematics Series document by Salzer (1951). An abbreviated version is given in Appendix A. $\mathrm{H}(\mathrm{n})$ may also be read directly from the table provided in Appendix B.

Now

$$H^2(n) = (2/12) \left(\frac{\Gamma(6.5)}{\Gamma(6)}^2\right) = .9592$$

and

$$\hat{H}(\hat{v}^*) = .9888$$
.

Entering Appendix B with .9888 and interpolating between .9887 and .9890 yields \hat{v}^* = 22.17. From DiDonato and Hageman (1977), obtain

$$\chi^2_{0*,.025} = 11.10$$

$$\chi^2_{0*,.975} = 37.00$$

via interpolation. An approximate 95% confidence interval for CEP using the fourth estimator is, therefore, given by

$$\left(\frac{232.78}{(37.00/22.17)^{\frac{1}{2}}} < CEP < \frac{232.78}{(11.10/22.17)^{\frac{1}{2}}}\right)$$

or

be modified to read

One notes that these two intervals are different. Had the other three estimators been used to construct confidence intervals, they too would have been different. We now have the problem of deciding which estimator to use for constructing confidence intervals. This will be discussed in the next chapter.

Before leaving this chapter, something needs to be said regarding the assumption of zero means. Throughout the development in the report, it has been assumed that the errors have zero mean in both directions. An error has been assumed to be a miss distance from a target, and zero mean implies there is no bias, i.e., the target coincides with the distribution mean. There are applications where the errors are not miss distances, per se, but deviations from the mean impact point. This occurs when there is bias in either or both directions or when there is no target, i.e., the firings are conducted to estimate dispersion without regard to a target. In either case, the impact distribution is no longer centered on the target but on an unknown point $(\mu_{\rm x}, \mu_{\rm y})$, and CEP is the radius of the 50% circle which is centered on this point vice the target. To apply the methodology in this report to these cases, the squares of s and s in (3.4) must

$$s_{x}^{2} = \hat{\sigma}_{x}^{2} = \frac{\sum_{i=1}^{n} (x_{i} - \bar{x})^{2}}{n - 1} = \frac{\sum_{i=1}^{n} x_{i}^{2} - (\sum_{i=1}^{n} x_{i})^{2}/n}{n - 1}$$

$$s_{y}^{2} = \hat{\sigma}_{y}^{2} = \frac{\sum_{i=1}^{n} (y_{i} - \bar{y})^{2}}{n - 1} = \frac{\sum_{i=1}^{n} y_{i}^{2} - (\sum_{i=1}^{n} y_{i})^{2}/n}{n - 1}.$$
(5.4)

In (5.4), \bar{x} and \bar{y} are the averages of the impact point locations in the x and y directions, respectively. In addition, the degrees of freedom associated with each estimator must be reduced by replacing n with n - 1 in each as follows:

$\begin{array}{c} \underline{\text{ESTIMATOR}} \\ \text{CEP}_1 \\ \text{CEP}_3 \\ \text{CEP}_5 \\ \end{array} \qquad \qquad \begin{array}{c} \text{MODIFIED d.f. FOR NON-ZERO MEANS} \\ \text{2 (n - 1)} \\ \text{(n - 1)} \\ \text{CEP}_5 \\ \\ \text{CEP}_4 \\ \end{array} \qquad \qquad \begin{array}{c} \text{H}(\upsilon^{\frac{1}{2}}) = \begin{bmatrix} 1 - \left\{ 1 - H^2 \left(n - 1 \right) \right\} \frac{\left(a_1^2 \sigma_X^2 + a_2^2 \sigma_Y^2 \right)}{\left(a_1 \sigma_X + a_2 \sigma_Y \right)^2} \end{bmatrix}^{\frac{1}{2}} \\ \text{CEP}_4 \\ \end{array}$

This reduction in degrees of freedom means a slight reduction in precision. In effect, it requires n + 1 deviations from the mean to provide the same precision as n miss distances.

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CHAPTER 6

MONTE CARLO VERIFICATION

To ascertain if the formulated approximations produced confidence intervals with confidence close to 1 - α , a Monte Carlo simulation was written for the CDC 6700. This would also provide a means of comparing the estimators with respect to their confidence level and their expected confidence interval length. One replicate of the simulation entailed generating a sample of n miss distances from a bivariate normal distribution with zero mean and variances σ_x^2 and σ_x^2 . These n values were then used to compute a CEP confidence interval using the five estimators $\widehat{\text{CEP}}_1$ to $\widehat{\text{CEP}}_5$. The length of each interval was computed, and for each interval, it was determined whether the interval contained the true (population) CEP. This process was replicated N = 10,000 times. The proportion of replicates in which the confidence interval contained the true CEP provided an estimate of the confidence associated with each estimator, and the average interval length for each provided an estimate of the expected length.

The values of the parameters used in the simulation are:

n = number of miss distances = sample size = 5, 10, 20

N = number of replicates = 10,000

 $1 - \alpha = nominal confidence level = .95$

$$c = \sigma_{\min}/\sigma_{\max} = 1.0, .75, .50, .35, .20, .05.$$

It was necessary to run a large number of replicates to ensure results with reasonable precision. The 10,000 replicates used provided estimates of confidence with an error of less than .01 with probability .95. Because of the large N, the sample sizes were restricted to small values to keep the computer time within bounds. A nominal value of $\alpha=.05\ (\Longrightarrow)$ a nominal confidence level of .95) was used in the construction of all confidence intervals within the simulation. It follows that if the confidence intervals were exact (vice approximate), the Monte Carlo confidence estimates should be within .01 of .95 or .95 \pm .01 with probability .95. Hence, any confidence estimate which departs seriously from .95 \pm .01 will reflect poorly on the estimator which produced it. One additional comment is required before discussing the results. The simulated confidence levels depend only on the ratio of the sigmas so that it was not necessary to vary both standard deviations. The larger was designated σ and set equal to unity while the smaller was designated $\sigma_{\rm x}$ and set equal to the ratio c. While the average confidence interval lengths are dependent on both sigmas, they were

only constructed for σ_x = c, σ_y = 1. This is all that is required for comparison purposes. If such lengths are needed for values of σ_x and σ_y other than c and 1, they can be obtained by multiplying the tabled entry for appropriate c by σ_y = σ_{max} .

The results of the simulations are set out in Tables 6-1 and 6-2. Let us first discuss the simulated confidence levels shown in Table 6-1. One first notes that all five estimators provide confidence within (or nearly within) the sampling variations $(\pm .01)$ of .95 when c = 1. This is the circular case and all the estimators except CEP₅ degenerate properly to the maximum likelihood estimator for CEP. Hence, the result that all do well for c = 1 is not unexpected. Next, one notes that as c departs from unity (that is, as the impact distribution departs from circularity), the confidence associated with CEP $_{
m 1}$ departs seriously from .95. For example, with n = 10 and c = .20 (5 to 1 ratio of the sigmas) the confidence associated with $\mathtt{CEP_1}$ is only .689. This means that if one were to use circular theory to construct a 95% confidence interval for CEP when the distribution was elliptical with a 5 to 1 ratio of the sigmas, his interval would have confidence of less than .7! This rules out CEP1 unless one is nearly certain that the impact distribution is circular normal. This result is also not unexpected, but it does quantify how poorly the circular estimator performs in the elliptical case.

In general, the others do reasonably well unless c is small. One notes this especially for CEP_2 when c = .05; the confidence falls from .930 for n = 5 to .912 for n = 20. It would continue to decrease as n increases due to the error in CEP approximation for small c (see Figure 3-2). The distribution of CEP $_2$ becomes more concentrated about the approximate CEP as n increases. If the approximation is in serious error (which it is for small c), then the distribution is concentrated about the wrong value. The simulation was run for n = 100 at c = .05 with a resulting confidence estimate of only .714. We see the same behavior at larger c values but to a lesser extent. For example, at c = .35, the confidence estimate is .942 for n = 20 but dips to .922 for n = 100. The upshot here is that \mbox{CEP}_2 would be a problem for small c or even moderate c if the sample is large enough. With regard to CEP $_3$, one sees that small values of c pose no problem. In fact, the confidence for CEP3 is asymptotic to .95 at c = 0. Also, for values of c around .5, the confidence estimates are slightly higher than .95. It tends to peak out at about .97. Selected runs for n=100show that this result changes very little with n. There is a slight price to pay for this extra confidence, and this will be addressed when Table 6-2 is discussed. CEP₄ provides confidence close to .95 for all values of c except those where CEP₄ departs from CEP (see Figure 3-4). At those values, there is a reduction in confidence which increases with n but not as severely as for CEP₂. The performance of CEP₅ is not poor with respect to confidence. However,

TABLE 6-1. SIMULATED CONFIDENCE LEVELS

		n = 5			
C	ĈEP ₁	CEP ₂	$\hat{\text{CEP}_3}$	$\hat{\text{CEP}_4}$	ĈEP ₅
1.0 .75 .50 .35 .20	.950 .941 .894 .830 .753	.947 .947 .941 .937 .932	.963 .965 .968 .963 .952	.946 .945 .944 .939 .923	.963 .965 .967 .961 .950
		10			
		n = 10			
<u>C</u>	CÊP ₁	ĈEP2	ĈÊP3	CÊP4	CEP ₅
1.0 .75 .50 .35 .20	.947 .935 .876 .789 .689	.945 .944 .941 .939 .939	.955 .958 .967 .967 .959	.944 .943 .943 .941 .931 .943	.955 .959 .966 .965 .955
		n = 20			
<u></u>	$\hat{\text{CEP}_1}$	$\hat{\text{CEP}_2}$	$\hat{\text{CEP}_3}$	CEP4	$\hat{\text{CEP}_5}$
1.0 .75 .50 .35 .20	.952 .938 .858 .724 .567	.952 .951 .945 .942 .946	.956 .960 .970 .970 .961 .950	.951 .951 .948 .947 .937	.956 .960 .969 .968 .955

TABLE 6-2. AVERAGE CONFIDENCE INTERVAL LENGTHS

	n = 5						
<u> </u>	CEP ₁	$\hat{\text{CEP}_2}$	CEP3	ĈEP4	CEP ₅		
1.0 .75 .50 .35 .20	1.213 1.071 .950 .897 .856	1.160 1.028 .923 .889 .876	1.305 1.175 1.118 1.129 1.149 1.176	1.145 1.014 .918 .917 .985 1.054	1.317 1.186 1.131 1.144 1.168 1.196		
		n =	10				
<u>C</u>	$\hat{\text{CEP}_1}$	$\hat{\mathtt{CEP_2}}$	CEP3	CEP4	ĈEP 5		
1.0 .75 .50 .35 .20	.792 .698 .622 .587 .564 .553	.776 .685 .614 .586 .573	.817 .735 .697 .693 .694 .695	.768 .676 .601 .586 .636	.823 .741 .705 .702 .706		
		n = 1	20				
<u>C</u>	$\hat{\text{CEP}_1}$	$\hat{\mathtt{CEP_2}}$	CEP ₃	ĈEP4	ĈEP ₅		
1.0 .75 .50 .35 .20	.537 .475 .423 .400 .384 .378	.533 .472 .421 .401 .388 .387	.545 .492 .465 .460 .455	.531 .467 .411 .393 .429	.549 .496 .470 .466 .462		

there is little rationale for its use in constructing confidence intervals. The Wilson-Hilferty approximation avoids the use of chi-square percentage points for fractional degrees of freedom in forming CEP₄. However, they are needed in the computation of the interval, so little effort is saved.

Let us now discuss the average confidence interval lengths in Table 6-2. As previously noted, these lengths depend on both $\boldsymbol{\sigma}_{\!_{\boldsymbol{X}}}$ and $\boldsymbol{\sigma}_{\!_{\boldsymbol{V}}}$ but were computed only not compare all five since some were eliminated as viable candidates in our discussions of Table 6-1. \texttt{CEP}_1 was eliminated because its confidence eroded seriously as c departed from unity. CEP₂ had a less serious but similar problem, and ${\tt CEP_5}$ was eliminated because it offered no improvement over ${\tt CEP_3}$ and only a slight reduction in computation. This leaves only $\mathtt{CEP_3}$ and $\mathtt{CEP_4}$ to discuss One notes that the average lengths are uniformly less for CEP4 than for At mid values of c, this is due in part to the inflated confidence inherent in the approximation of the distribution of CEP3, i.e., the higher the confidence, the longer the confidence length. However, not all of the difference in length can be attributed to higher confidence. A study by Taub and Thomas (1982) shows that the variance of ${\tt CEP_4}$ is less than the variance of ${\tt CEP_3}$, and this is the primary reason for the difference in length. Even so, CEP4 suffers from the bias caused by the error in approximation shown in Figure 3-4. This has an effect on the confidence level associated with CEP4 for some values of c, but it would not be appreciable for small n.

In summary, we can state that the logical choice lies between ${\rm CEP_3}$ and ${\rm CEP_4}$. The third holds for all values of c, regardless of n, and is easy to implement. The fourth offers somewhat shorter confidence lengths but it is cumbersome to implement and would provide a reduced confidence level for some values of n and c.

It would be highly desirable to have a CEP estimator with a variance as small or smaller than CEP4 which would have negligible bias for all 0 < c \leq 1, and which would avoid the cumbersomeness of a piece-wise linear function. The authors have several ideas along this line and hope to explore their merits in the near future.

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APPENDIX A

TABLE OF $\Gamma(n)$ AND $\Gamma(n+\frac{1}{2})$ FOR $n=1,\ldots 100$ Excerpted from National Bureau of Standards Applied Mathematics Series - 16

by

Herbert E. Salzer

n	n!	$\Gamma(n+\frac{1}{2})$	n	n!	$\Gamma(n+\frac{1}{2})$
0	1. 00000 00000 00000 (0)	1. 7724 539 (0)	50	3. 04140 93201 71338 (64)	4. 2904 629 (63)
1	1. 00000 00000 00000 (0)	8. 8622 693 (-1)	51	1. 55111 87532 87382 (66)	2. 1666 838 (65)
2	2. 00000 00000 00000 (0)	1. 3293 404 (0)	52	8. 06581 75170 94388 (67)	1. 1158 421 (67)
3	6. 00000 00000 00000 (0)	3. 3233 510 (0)	53	4. 27488 32840 60026 (69)	5. 8581 712 (68)
4	2. 40000 00000 00000 (1)	1. 1631 728 (1)	54	2. 30843 69733 92414 (71)	3. 1341 216 (70)
5	1. 20000 00000 00000 (2)	5. 2342 778 (1)	55	1. 26964 03353 65828 (73)	1. 7080 963 (72)
6	7. 20000 00000 00000 (2)	2. 8788 528 (2)	56	7. 10998 58780 48635 (74)	9. 4799 344 (73)
7	5. 04000 00000 00000 (3)	1. 8712 543 (3)	57	4. 05269 19504 87722 (76)	5. 3561 629 (75)
8	4. 03200 00000 00000 (4)	1. 4034 407 (4)	58	2. 35056 13312 82879 (78)	3. 0797 937 (77)
9	3. 62880 00000 00000 (5)	1. 1929 246 (5)	59	1. 38683 11854 56898 (80)	1. 8016 793 (79)
10	3. 62880 00000 00000 (6)	1. 1332 784 (6)	60	8. 32098 71127 41390 (81)	1. 0719 992 (81)
11	3. 99168 00000 00000 (7)	1. 1899 423 (7)	61	5. 07580 21387 72248 (83)	6. 4855 951 (82)
12	4. 79001 60000 00000 (8)	1. 3684 337 (8)	62	3. 14699 73260 38794 (85)	3. 9886 410 (84)
13	6. 22702 08000 00000 (9)	1. 7105 421 (9)	63	1. 98260 83154 04440 (87)	2. 4929 006 (86)
14	8. 71782 91200 00000 (10)	2. 3092 318 (10)	64	1. 26886 93218 58842 (89)	1. 5829 919 (88)
15	1. 30767 43680 00000 (12)	3. 3483 861 (11)	65	8. 24765 05920 82471 (90)	1. 0210 298 (90)
16	2. 09227 89888 00000 (13)	5. 1899 985 (12)	66	5. 44344 93907 74431 (92)	6. 6877 450 (91)
17	3. 55687 42809 60000 (14)	8. 5634 974 (13)	67	3. 64711 10918 18869 (94)	4. 4473 504 (93)
18	6. 40237 37057 28000 (15)	1. 4986 121 (15)	68	2. 48003 55424 36831 (96)	3. 0019 615 (95)
19	1. 21645 10040 88320 (17)	2. 7724 323 (16)	69	1. 71122 45242 81413 (98)	2. 0563 436 (97)
20	2. 43290 20081 76640 (18)	5. 4062 430 (17)	70	1. 19785 71669 96989 (100)	1. 4291 588 (99)
21	5. 10909 42171 70944 (19)	1. 1082 798 (19)	71	8. 50478 58856 78623 (101)	1. 0075 570 (101)
22	1. 12400 07277 77608 (21)	2. 3828 016 (20)	72	6. 12344 58376 88609 (103)	7. 2040 324 (102)
23	2. 58520 16738 88498 (22)	5. 3613 036 (21)	73	4. 47011 54615 12684 (105)	5. 2229 235 (104)
24	6. 20448 40173 32394 (23)	1. 2599 063 (23)	74	3. 30788 54415 19386 (107)	3. 8388 487 (106)
25	1. 55112 10043 33099 (25)	3. 0867 705 (24)	75	2. 48091 40811 39540 (109)	2. 8599 423 (108)
26	4. 03291 46112 66056 (26)	7. 8712 649 (25)	76	1. 88549 47016 66050 (111)	2. 1592 564 (110)
27	1. 08888 69450 41835 (28)	2. 0858 852 (27)	77	1. 45183 09202 82859 (113)	1. 6518 312 (112)
28	3. 04888 34461 17139 (29)	5. 7361 843 (28)	78	1. 13242 81178 20630 (115)	1. 2801 692 (114)
29	8. 84176 19937 39702 (30)	1. 6348 125 (30)	79	8. 94618 21307 82975 (116)	1. 0049 328 (116)
30	2. 65252 85981 21911 (32)	4. 8226 969 (31)	80	7. 15694 57046 26380 (118)	7. 9892 157 (117)
31	8. 22283 86541 77923 (33)	1. 4709 226 (33)	81	5. 79712 60207 47368 (120)	6. 4313 187 (119)
32	2. 63130 83693 36935 (35)	4. 6334 061 (34)	82	4. 75364 33370 12842 (122)	5. 2415 247 (121)
33	8. 68331 76188 11886 (36)	1. 5058 570 (36)	83	3. 94552 39697 20659 (124)	4. 3242 579 (123)
34	2. 95232 79903 96041 (38)	5. 0446 209 (37)	84	3. 31424 01345 65353 (126)	3. 6107 553 (125)
35	1. 03331 47966 38614 (40)	1. 7403 942 (39)	85	2. 81710 41143 80550 (128)	3. 0510 883 (127)
36	3. 71993 32678 99012 (41)	6. 1783 994 (40)	86	2. 42270 95383 67273 (130)	2. 6086 805 (129)
37	1. 37637 53091 22635 (43)	2. 2551 158 (42)	87	2. 10775 72983 79528 (132)	2. 2565 086 (131)
38	5. 23022 61746 66011 (44)	8. 4566 842 (43)	88	1. 85482 64225 73984 (134)	1. 9744 450 (133)
39	2. 03978 82081 19744 (46)	3. 2558 234 (45)	89	1. 65079 55160 90846 (136)	1. 7473 838 (135)
40	8. 15915 28324 78977 (47)	1. 2860 502 (47)	90	1. 48571 59644 81761 (138)	1. 5639 085 (137)
41	3. 34525 26613 16381 (49)	5. 2085 035 (48)	91	1. 35200 15276 78403 (140)	1. 4153 372 (139)
42	1. 40500 61177 52880 (51)	2. 1615 290 (50)	92	1. 24384 14054 64131 (142)	1. 2950 336 (141)
43	6. 04152 63063 37384 (52)	9. 1864 981 (51)	93	1. 15677 25070 81642 (144)	1. 1979 060 (143)
44	2. 65827 15747 88449 (54)	3. 9961 267 (53)	94	1. 08736 61566 56743 (146)	1. 1200 422 (145)
45	1. 19622 22086 54802 (56)	1. 7782 764 (55)	95	1. 03299 78488 23906 (148)	1. 0584 398 (147)
46	5. 50262 21598 12089 (57)	8. 0911 574 (56)	96	9. 91677 93487 09497 (149)	1. 0108 100 (149)
47	2. 58623 24151 11682 (59)	3. 7623 882 (58)	97	9. 61927 59682 48212 (151)	9. 7543 169 (150)
48	1. 24139 15592 53607 (61)	1. 7871 344 (60)	98	9. 42689 04488 83248 (153)	9. 5104 590 (152)
49	6. 08281 86403 42676 (62)	8. 6676 018 (61)	99	9. 33262 15443 94415 (155)	9. 3678 021 (154)
50	3. 04140 93201 71338 (64)	4. 2904 629 (63)	100	9. 33262 15443 94415 (157)	9. 3209 631 (156)

APPENDIX B

TABLES OF x AND H(x) FOR x = .1 TO 400

	н(х)	. 9569	. 9573	. 9577	. 9580	28	.9587	. 9590	. 9594	. 9597	. 9600	. 9603	. 9606	6096	9613	. 9615	. 9618	. 9621	. 9624	. 9627	. 9630	. 9632	. 9635	. 9638	. 9640	. 9643	. 9645	9648	9656	5668.	. 9655	. 9657	. 9660	.9662	. 9664	. 9667	9669	. 96/1
	×	5.65	5.70	5.75	5.80	5.85	5.90	5.95	9.00	6.05	6.10	6.15	6.20	6.25	6.30	6.35	6.40	6.45	6.50	6.55	6.60	6.65	6.70	6.75	6.80	6.85	6.90	6.95	9.7	7.05	7.10	7.15	7.20	7.25	7.30	7.35	7.40	7.45
	H(X)	9370	37	. 9385	. 9393	.9400	.9407	4	42	42	43	44	44	.9452	.9458	.9464	.9469	.9475	.9480	.9486	.9491	.9496	. 9501	.9506	.9511	. 9515	. 9520	. 9524	. 9529	. 9533	. 9538	.9542	.9546	. 9550	. 9554	. 9558	.9562	. 9566
TABLE 1	×				3.95	•			۲,	4.20	4.25	ω.	4.35	•	4.45													5.10						4	4	5.50	Л	φ.
-	H(X)	8837	8862	.8887	.8911	.8933	.8955	.8976	9668.	. 9015	. 9034	. 9052	6906	. 9086	.9102	.9118	.9133	.9147	.9161	.9175	.9188	.9201	. 9213	. 9225	.9237	. 9248	. 9259	. 9270	.9280	. 9290	. 9300	. 9310	. 9319	. 9328	. 9337	. 9345	. 9354	. 9362
	×				2.10																				•			•	•			•	•					
	H(X)	0	37.12	4950	. 5386	5748	.6056	.6322	. 6555	.6760	6942	7105	7252	7385	.7507	.7617	.7719	. 7812	. 7899	. 7979	. 8053	. 8122	8187	8247	8304	.8357	.8407	.8454	.8499	.8541	. 8581	.8619	. 8654	.8689	.8721	.8752	.8781	.8810
	×	ç	٠ پ		200	30	35	40	45	50		60.		02:	7.5	80	85	06	96.	8	1.05	1.10	 	1 20		1.30	1.35	•	1.45	•	1.55	1.60	1.65	1.70	1.75	1.80	1.85	1.90

X H(X) X X H(X) X X H(X) X X H(X) X X X X X X X					TABLE 1			
50 9673 9.35 .9737 16.00 .9845 31.00 50 9675 9.40 .9738 16.25 .9847 32.00 65 .9677 9.40 .9738 16.50 .9847 32.00 65 .9681 9.55 .9742 17.50 .9858 34.00 77 .9683 9.75 .9743 17.50 .9856 34.00 86 .9684 9.75 .9743 17.50 .9858 36.00 90 .9683 9.75 .9747 18.25 .9866 41.00 90 .9693 9.85 .9747 18.25 .9866 41.00 90 .9694 9.95 .9747 18.25 .9866 41.00 90 .9695 9.90 .9754 18.25 .9866 41.00 10 .9695 9.90 .9754 18.25 .9866 41.00 11 .9695 .9750 .9754	×	H(X)	×	H(X)	×	H(X)	×	H(X)
550 9673 9.35 9731 16.25 9874 9.35 560 9677 9.45 9731 16.25 9874 32.00 65 9677 9.45 9739 16.25 9854 32.00 77 9683 9.56 9742 17.05 9854 32.00 86 9673 9.45 9742 17.25 9854 35.00 87 9683 9.75 9745 17.25 9856 37.00 96 9683 9.75 9745 17.25 9866 37.00 96 976 9746 17.75 9866 41.00 96 96 9746 17.75 9866 41.00 97 96 975 18.75 9868 43.00 96 97 975 18.75 9868 43.00 10 98 975 18.75 9868 43.00 11 12 975 18.75 </td <td></td> <td></td> <td></td> <td>i d</td> <td></td> <td>0 7 7</td> <td></td> <td>0666</td>				i d		0 7 7		0666
65 9877 9.45 9738 16.25 9887 9.50 65 9877 9.45 9741 16.25 9882 35.00 70 9881 9.50 9741 16.50 9882 37.00 80 9683 9.60 9742 17.00 9885 37.00 80 9683 9.60 9742 17.00 9885 37.00 90 9683 9.60 9744 17.25 9886 37.00 90 9693 9.75 9747 18.05 9863 39.00 90 9.60 9747 18.25 9866 47.00 90 9.74 18.25 9866 47.00 90 9.75 18.25 9866 47.00 10 9.85 9.75 19.25 9866 47.00 10 9.86 9.75 19.25 9867 47.00 10 9.86 9.75 19.25 9874		. 9673		18/8.				9922
660 98677 9.45 9739 16.50 9880 34.00 75 9681 9.50 9744 16.75 9854 35.00 75 9681 9.50 9742 17.00 9854 35.00 86 9.65 9744 17.50 9858 37.00 90 9887 9.75 9747 18.00 3854 37.00 90 9887 9.75 9744 18.00 9858 37.00 90 9883 9.75 9747 18.00 9864 40.00 96 9.60 9.74 18.75 9868 37.00 96 9.60 9.75 18.75 9868 42.00 96 9.60 9.75 19.00 9868 42.00 96 9.60 9.75 19.00 9868 42.00 96 9.60 9.75 19.00 9868 42.00 96 9.70 10.00 97.20		. 9675		. 9738		488.		4000
65 9679 9 50 9741 16.75 9852 34.00 70 9681 9.50 9742 17.25 9854 35.00 80 9683 9.65 9742 17.25 9854 35.00 80 9683 9.65 9744 17.25 9856 39.00 90 9683 9.75 9744 18.00 9864 40.00 95 9691 9.70 9749 18.25 9864 40.00 96 9.693 9.90 9751 18.75 9868 42.00 10 9.693 9.90 9751 18.75 9868 42.00 10 9.90 9.74 18.75 9868 42.00 10 9.90 9.75 19.25 19.00 9878 41.00 10 9.90 9.75 19.25 19.00 9868 42.00 10 9.90 9.75 19.75 19.75 19.70 19.70		. 9677		. 9739		0586.		. 0000
77 9681 9.55 9742 17.00 9854 35.00 75 9683 9.60 9743 17.25 9854 35.00 85 96887 9.70 9749 17.50 9856 37.00 96 9689 9.75 9749 18.25 9864 40.00 96 9689 9.75 9750 18.25 9864 40.00 96 9697 9.85 9751 18.25 9866 41.00 10 9697 9.95 9751 18.75 9868 42.00 10 9697 9.75 19.25 9866 41.00 10 9699 10.00 9751 19.25 9874 40.00 10 9700 10.25 9759 19.25 9874 40.00 10 9700 11.25 9776 20.00 9874 40.00 10 9700 11.25 9781 21.50 9874 40.00<		. 9679		. 9741		. 9852		1288.
7.5 9.60 94.43 17.25 9856 36.00 80 9685 9.65 9745 17.25 9856 36.00 80 9687 9.75 9747 18.00 9864 40.00 96 9.69 9.75 9749 18.25 9864 40.00 96 9.695 9.90 9751 18.25 9864 40.00 96 9.92 9.75 19.00 9864 40.00 96 9.95 9.95 9751 18.25 9864 40.00 10 9.95 9.95 9.75 19.00 9868 42.00 11 9.95 9.75 19.00 9874 42.00 10 9.95 9.70 19.25 9874 45.00 10 9.95 9.70 19.25 9874 46.00 10 9.95 9.70 19.25 9874 46.00 10 9.95 9.70 9.70	•	9681		. 9742		. 9854		9929
9685 9745 17.50 9868 37.00 86 9687 9.65 9746 17.50 9868 37.00 96 9687 9.75 9746 17.50 9868 37.00 96 9691 9.85 9750 18.25 9864 40.00 96 9.95 9751 18.25 9868 42.00 10 9697 9.95 9752 19.60 9873 42.00 10 9697 9.95 9752 19.50 9873 42.00 10 9.95 9752 19.50 9873 42.00 20 9700 10.00 9775 47.00 9873 42.00 20 9700 11.00 9776 20.00 9874 45.00 30 9704 11.00 9776 20.00 9887 46.00 31 970 9776 20.00 9887 47.00 30 971 11.25	•	9683		.9743		. 9856	36.00	. 9931
85 966 38.00 96 97 974 11.75 9860 38.00 96 96 97 974 18.25 9864 40.00 96 9693 9.75 974 18.50 9866 40.00 96 9693 9.90 9750 18.25 9866 40.00 10 9693 9.90 9754 18.25 9868 42.00 10 9699 10.00 9754 19.25 9873 40.00 20 9700 9754 19.25 9874 40.00 20 9700 9754 19.50 9876 40.00 30 9704 10.00 9776 20.00 9876 40.00 30 9704 11.00 9776 20.00 9876 40.00 40 9707 11.50 9786 20.00 9876 40.00 40 9707 11.50 9786 20.00 <t< td=""><td></td><td>9685</td><td></td><td>.9745</td><td></td><td>. 9858</td><td>37.00</td><td>. 9933</td></t<>		9685		.9745		. 9858	37.00	. 9933
96 96 96 97<		9687		.9746		. 9860	38.00	. 9934
95 96 97<		6896		.9747		. 9862	39.00	. 9936
05 9693 9.85 9.750 18.50 9866 41.00 05 9695 9.90 9751 18.75 9868 42.00 16 9697 9.95 9.752 19.00 9868 42.00 20 9697 10.05 9754 19.25 9874 44.00 20 9700 10.25 9776 20.00 9874 46.00 25 9702 10.75 9776 20.00 9874 46.00 35 9704 10.75 9776 20.00 9874 47.00 36 9704 11.50 9785 21.50 9887 49.00 40 9712 11.75 9794 22.00 9887 60.00 55 9712 12.25 9802 22.00 9889 10.00 65 9714 12.25 9802 22.00 9889 10.00 70 9714 12.25 9802 22.00	•	9691		.9749		. 9864	40.00	. 9938
05 9695 9751 18.75 9868 42.00 10 9697 9.95 9752 19.00 9869 42.00 15 9699 10.20 9754 19.25 9871 44.00 25 9700 10.25 9770 20.00 9874 45.00 26 9702 10.50 9776 10.50 9874 47.00 30 9704 10.25 9770 20.00 9874 47.00 45 9704 11.25 9781 21.00 9882 49.00 45 9711 11.25 9784 22.00 9884 50.00 50 9712 11.25 9794 22.50 9880 40.00 55 9712 12.00 9874 20.00 9884 50.00 55 9712 12.00 9784 20.00 9880 90.00 60 9714 12.00 9806 24.00 9894 1		- 696		.9750		9886		. 9939
10 9697 9.95 9752 19.00 9869 43.00 15 9697 10.00 9754 19.25 9871 44.00 20 9700 10.50 9759 19.75 9874 44.00 20 9702 10.50 9776 20.00 9874 46.00 35 9704 10.75 9770 20.00 9874 46.00 35 9704 11.50 9776 20.00 9879 47.00 40 9707 11.50 9781 21.50 9887 49.00 50 9711 11.75 9790 22.50 9887 49.00 50 9711 11.75 9794 22.50 9887 40.00 50 9714 12.50 9802 23.50 9887 40.00 65 9714 12.50 9802 23.50 9889 110.00 70 9714 12.50 9817 25.00 <th< td=""><td></td><td>2606.</td><td></td><td>9751</td><td></td><td>. 9868</td><td></td><td>. 9941</td></th<>		2606.		9751		. 9868		. 9941
15 9699 10.00 9754 19.25 9871 44.00 20 9700 10.25 9759 19.50 9873 45.00 20 9702 10.50 9759 19.50 9874 45.00 30 9704 10.75 9776 20.00 9874 46.00 40 9706 11.00 9776 20.00 9879 48.00 40 9707 11.25 9781 21.00 9882 49.00 45 9709 11.50 9784 22.00 9887 60.00 55 9714 11.50 9794 22.50 9894 40.00 60 9714 12.25 9802 24.00 9894 40.00 65 9714 12.75 9802 24.50 9894 40.00 65 9714 12.75 9802 24.50 9894 100.00 75 972 13.00 9813 25.00 <td< td=""><td></td><td>7696</td><td></td><td>9752</td><td></td><td>. 9869</td><td></td><td>.9942</td></td<>		7696		9752		. 9869		.9942
15 9700 10.25 9759 19.50 9873 45.00 25 9700 10.75 9765 19.75 9874 46.00 30 9704 10.75 9776 20.50 9874 46.00 30 9704 11.26 9781 21.50 9882 49.00 45 9709 11.50 9785 21.50 9882 49.00 45 9709 11.75 9784 22.50 9884 50.00 50 9711 17.75 9794 22.50 9887 49.00 60 9714 12.25 9798 23.00 9894 90.00 65 9714 12.25 9798 23.00 9894 90.00 65 9716 12.50 9802 24.50 9894 100.00 65 9718 12.50 9814 10.00 9896 100.00 70 9719 13.50 9813 25.00 <	٠	6090		9754		.9871		.9943
25 9702 10.50 9765 19.75 .9874 46.00 35 9704 10.75 9776 20.00 .9876 47.00 35 9704 10.75 9776 20.00 .9879 47.00 35 9705 11.50 9781 21.50 .9887 49.00 40 9709 11.50 9784 22.00 .9887 49.00 55 9712 12.00 9784 22.50 .9887 60.00 55 9714 12.50 9782 22.50 .9894 100.00 60 9714 12.50 9802 22.50 .9894 100.00 65 9716 12.50 9802 22.50 .9894 100.00 75 9719 13.00 .9810 24.50 .9894 100.00 75 9720 13.50 .9817 25.50 .9904 140.00 95 9724 13.75 .9826 27.	•	0070		9759		.9873		.9945
35 9704 10.75 9770 20.00 9876 47.00 35 9704 11.25 9776 20.50 9879 48.00 40 9707 11.25 9781 21.50 9882 48.00 45 9709 11.50 9784 22.50 9887 60.00 55 9712 12.00 9794 22.50 9887 60.00 65 9714 12.25 9802 22.50 9894 90.00 65 9714 12.75 9802 23.50 9894 100.00 75 9714 12.75 9802 24.00 9894 100.00 75 9719 13.00 9813 25.50 9894 100.00 75 9719 13.00 9813 25.50 9894 100.00 75 972 13.50 9813 25.50 9904 140.00 85 972 14.00 9826 27.50		2078		9765		.9874		. 9946
9776 11.00 9776 20.50 9879 48.00 40 9700 11.25 9781 21.00 9882 49.00 40 9700 11.50 9785 21.00 9887 60.00 50 9711 11.75 9794 22.50 9897 70.00 65 9712 12.25 9802 23.50 9890 70.00 65 9714 12.25 9802 23.50 9894 90.00 65 9714 12.25 9802 24.50 9894 100.00 65 9716 12.75 9806 24.50 9899 110.00 77 9719 13.00 9813 25.00 9901 120.00 86 9720 13.50 9813 25.00 9904 140.00 87 9724 13.75 9820 26.50 9908 175.00 97 14.25 9820 27.50 9908 175.00		9704		0776.		.9876		. 9947
40 9707 11.25 9781 21.00 9882 49.00 45 9709 11.50 9785 21.50 9884 50.00 45 9709 11.50 9785 21.50 9887 60.00 55 9714 12.26 9798 22.00 9887 70.00 60 9714 12.25 9802 23.50 9894 90.00 60 9714 12.75 9806 24.00 9894 90.00 75 9717 12.75 9806 24.00 9894 100.00 75 9719 13.00 9813 25.00 9899 110.00 80 9720 13.50 9813 25.00 9904 140.00 90 9724 13.75 9820 26.50 9908 175.00 95 9727 14.25 9823 27.50 9908 175.00 95 9728 14.50 9829 27.50		9026		9776		. 9879	œ.	. 9948
45 9709 11.50 9785 21.50 9884 50.00 50 9711 11.75 9794 22.00 9887 60.00 55 9712 12.00 9794 22.50 9887 70.00 65 9714 12.25 9802 23.50 9894 90.00 70 9716 12.75 9802 23.50 9894 90.00 70 9717 12.75 9802 24.00 9899 100.00 75 9719 13.00 9813 25.00 9899 110.00 80 9720 13.50 9817 25.00 9901 120.00 85 9724 13.50 9820 140.00 9904 140.00 90 9724 14.00 9823 26.50 9908 175.00 90 9724 14.50 9826 27.00 9911 250.00 10 9730 14.75 9835 29.00		9707	•	.9781		. 9882		.9949
50 9711 11.75 9790 22.00 9887 60.00 55 9712 12.25 9794 22.50 9890 70.00 60 9714 12.25 9802 23.00 9892 80.00 65 9714 12.50 9802 23.50 9894 90.00 70 9717 12.75 9806 24.00 9894 100.00 75 9719 13.00 9813 25.00 9809 110.00 85 9722 13.50 9817 25.50 9904 140.00 96 9724 13.75 9820 26.00 9904 140.00 97 9724 14.00 9823 26.50 9904 150.00 95 9724 14.00 9823 27.50 9908 175.00 96 9727 14.25 9826 27.50 9908 175.00 97 16 973 14.75 9832		6076		.9785		. 9884		. 9950
55 9712 12.00 9794 22.50 9890 70.00 65 9714 12.25 9798 23.00 9892 80.00 65 9714 12.25 9802 23.00 9894 90.00 70 9716 12.50 9802 24.00 9894 90.00 70 9717 12.75 9806 24.00 9896 100.00 75 9720 13.25 9817 25.00 9901 120.00 80 9724 13.75 9820 26.00 9902 130.00 95 9724 14.00 9823 26.00 9904 140.00 95 9724 14.25 9826 27.00 9908 175.00 95 9724 14.25 9826 27.00 9908 175.00 96 9727 14.25 9829 27.50 9911 225.00 10 9730 14.75 9832 28.00	•	9711		.9790		. 9887		8966.
60 9714 12.25 9798 23.00 9892 80.00 65 9714 12.50 9802 23.50 9894 90.00 70 9717 12.75 9806 24.00 9896 100.00 75 9719 13.00 9810 24.50 9899 110.00 80 9720 13.25 9813 25.00 9901 120.00 85 9724 13.75 9820 26.00 9902 140.00 95 9724 13.75 9820 26.00 9904 140.00 95 9724 14.00 9823 26.50 9906 150.00 95 9725 14.00 9826 27.00 9906 175.00 97 9728 14.50 9829 27.50 9908 175.00 97 10 9730 14.75 9832 28.00 9911 250.00 15 9734 15.00 9835		97.12		.9794		0686.		. 9964
65 9716 12.50 9802 23.50 9894 90.00 997 70 9717 12.75 9806 24.00 9896 100.00 997 75 9719 13.00 9810 24.50 9899 110.00 997 80 9720 13.25 9813 25.00 9901 120.00 998 95 9724 13.55 9820 26.50 9904 140.00 998 95 9724 14.00 9823 26.50 9906 175.00 998 90 9728 14.00 9829 27.00 9908 175.00 998 90 9728 14.50 9829 27.50 9908 175.00 998 10 9730 14.75 9832 28.00 9911 250.00 999 15 9731 15.00 9840 29.50 9914 300.00 999 20 9734 15.75 <td< td=""><td>•</td><td>9714</td><td></td><td>.9798</td><td>е С</td><td>. 9892</td><td></td><td>6966</td></td<>	•	9714		.9798	е С	. 9892		6966
70 9717 12.75 9806 24.00 9896 100.00 997 75 9719 13.00 9810 24.50 9899 110.00 997 80 9720 13.25 9813 25.00 9901 120.00 997 85 9722 13.50 9817 25.50 9902 130.00 998 90 9724 13.75 9820 26.00 9904 140.00 998 95 9725 14.00 9823 26.50 9908 175.00 998 90 9727 14.50 9826 27.00 9908 175.00 998 10 9728 14.50 9835 28.00 9911 225.00 998 10 9730 15.25 9838 29.00 9914 300.00 999 15 9734 15.50 9840 29.50 9914 300.00 999 25 9734 15.75 <t< td=""><td></td><td>97.16</td><td></td><td>.9802</td><td>ω,</td><td>. 9894</td><td></td><td>. 9972</td></t<>		97.16		.9802	ω,	. 9894		. 9972
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$\label{eq:APPENDIX} \mbox{ C}$ THE CHI DISTRIBUTION

A discussion of the chi-square probability distribution can be found in most probability and statistics textbooks. It is a special case of the more general gamma distribution and its density function is given by

$$f_{X}(x) = \frac{1}{\Gamma(\frac{n}{2}) 2^{n/2}} x^{n/2 - 1} e^{-x/2}, 0 < x < \infty$$
.

Rarely, however, is the CHI distribution discussed in detail. Because this distribution is critical to the development of the approximate distributions for $\hat{\text{CEP}}_2$ and $\hat{\text{CEP}}_4$, the following is a brief introduction to the CHI distribution.

If X is defined as a chi-square random variable, then Y = \sqrt{X} is distributed as a CHI random variable whose density function is written as

$$f_{Y}(y) = \frac{2}{\Gamma(\frac{n}{2})2^{\frac{n}{2}-1}} x^{n-1} e^{\frac{-x^{2}}{2}}$$
, $0 < x < \infty$.

The mean of Y is given by

$$E(Y) = \frac{\Gamma(\frac{n+1}{2})2^{\frac{1}{2}}}{\Gamma(\frac{n}{2})}$$

and the variance of Y is given by

$$V(Y) = n - 2 \left[\frac{\Gamma\left(\frac{n+1}{2}\right)}{\Gamma\left(\frac{n}{2}\right)} \right]^{2}.$$

In general, the rth moment of Y is given by

$$E(Y^{r}) = \frac{\Gamma(\frac{n+r}{2})2^{r/2}}{\Gamma(\frac{n}{2})}.$$

If s is the sample standard deviation with υ degrees of freedom, then the previous results can be used to establish that

$$E(s) = \sqrt{\frac{2}{\upsilon}} \frac{\Gamma(\frac{\upsilon + 1}{2})}{\Gamma(\frac{\upsilon}{2})}$$

and

$$V(s) = \sigma^2 - \frac{2\sigma^2}{\upsilon} \left\{ \frac{\Gamma\left(\frac{\upsilon + 1}{2}\right)}{\Gamma\left(\frac{\upsilon}{2}\right)} \right\}^2 .$$

These results are needed to determine the degrees of freedom associated with $\widehat{\text{CEP}}_2$ and $\widehat{\text{CEP}}_4$. Additional information on the CHI distribution may be found in Krutchkoff (1970).

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